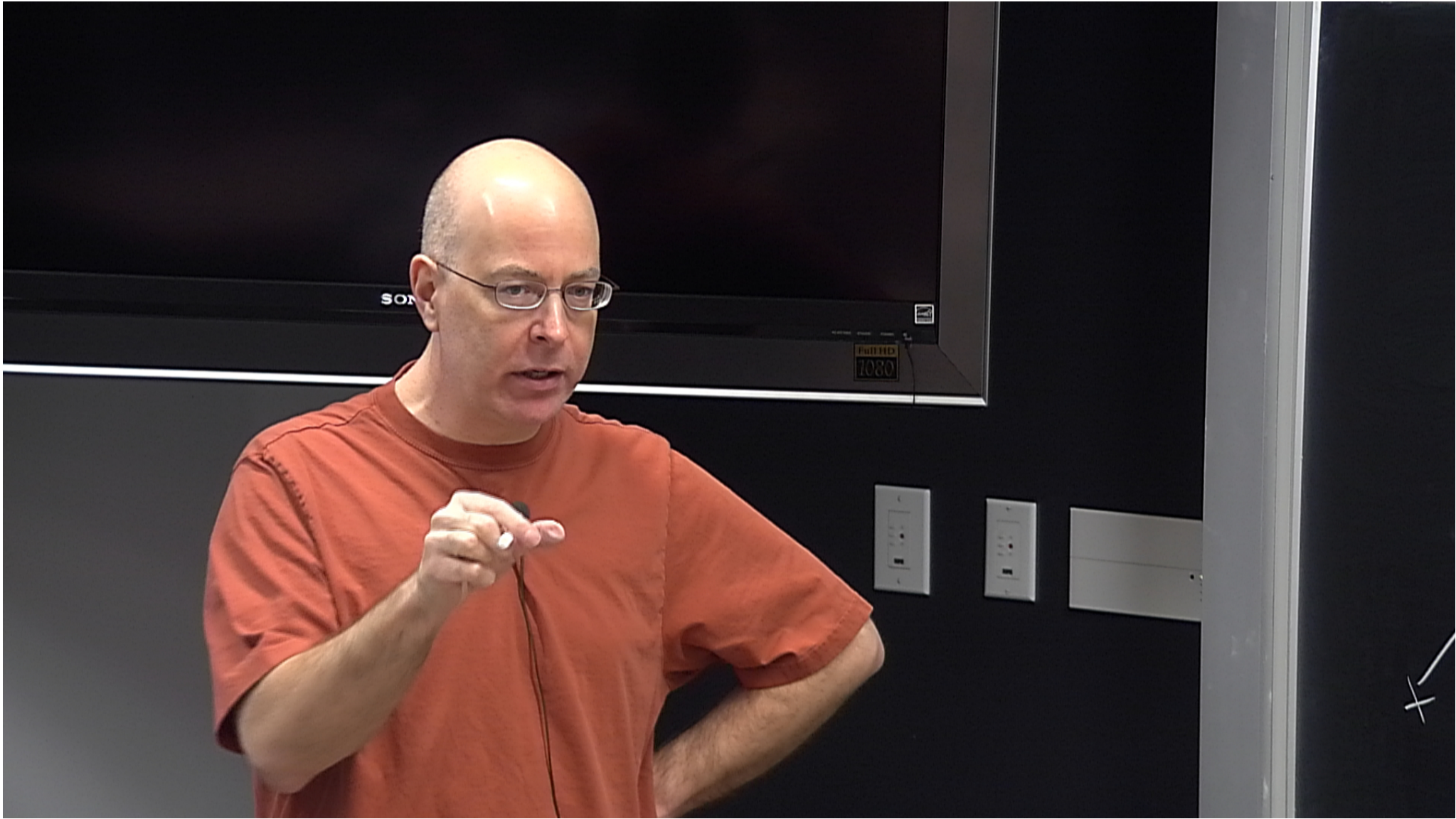


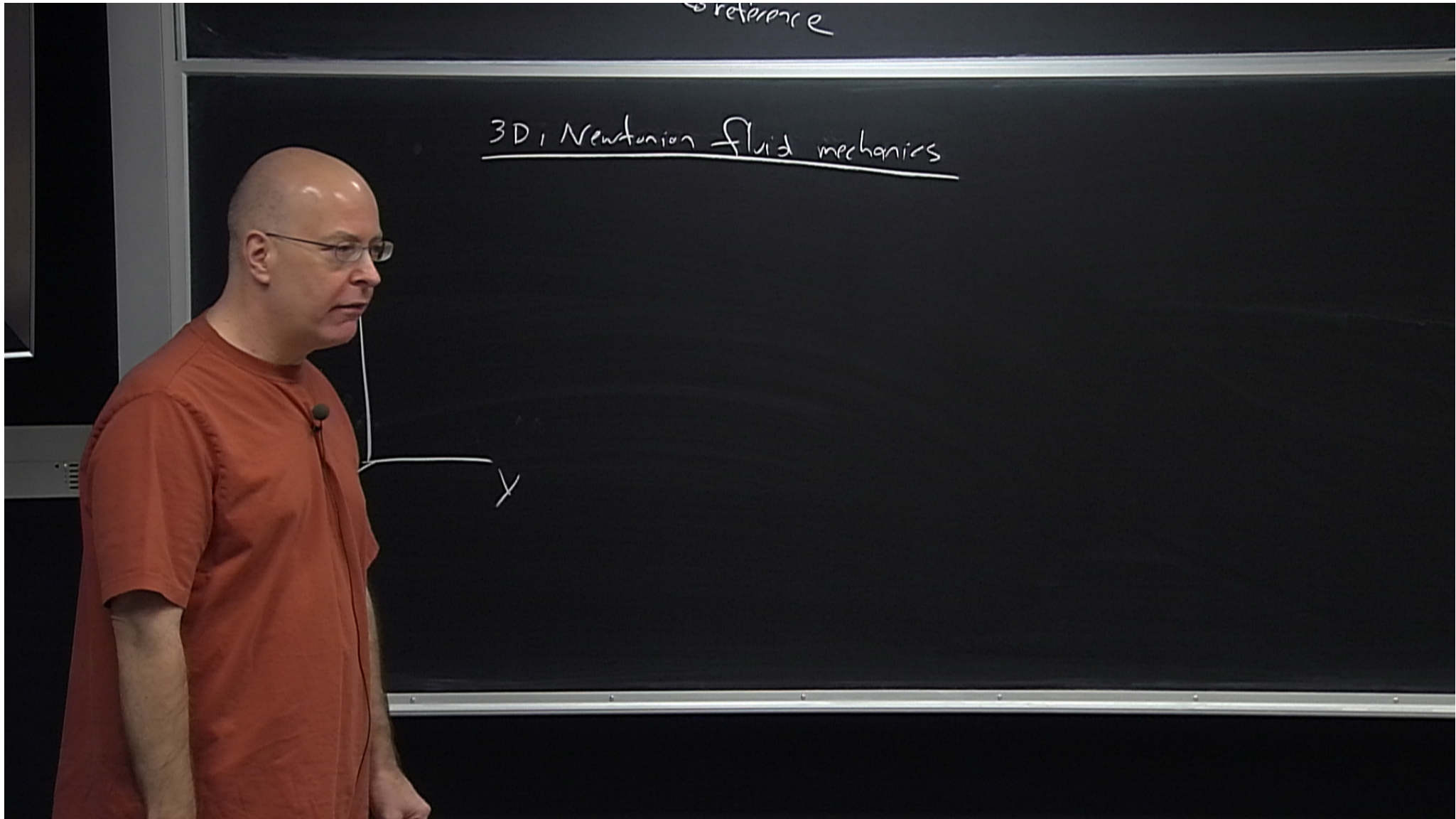
Title: Advanced General Relativity - Lecture 5

Date: Jan 25, 2012 10:00 AM

URL: <http://pirsa.org/12010153>

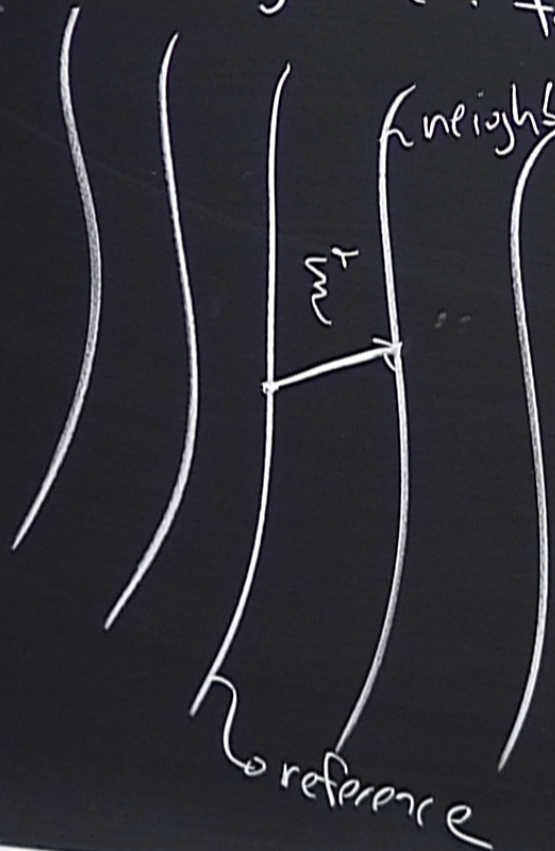
Abstract:



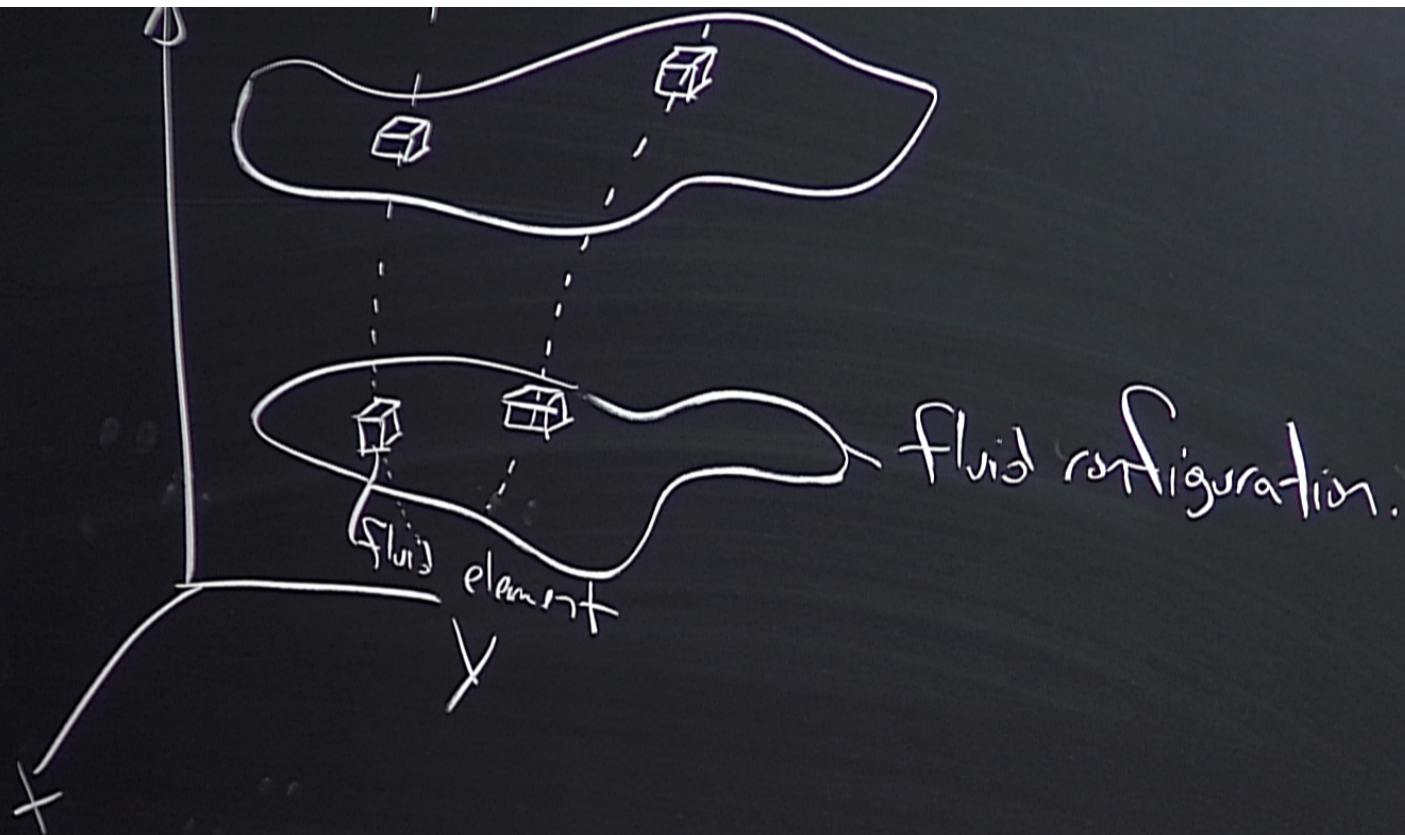


GEODESIC CONGRUENCES

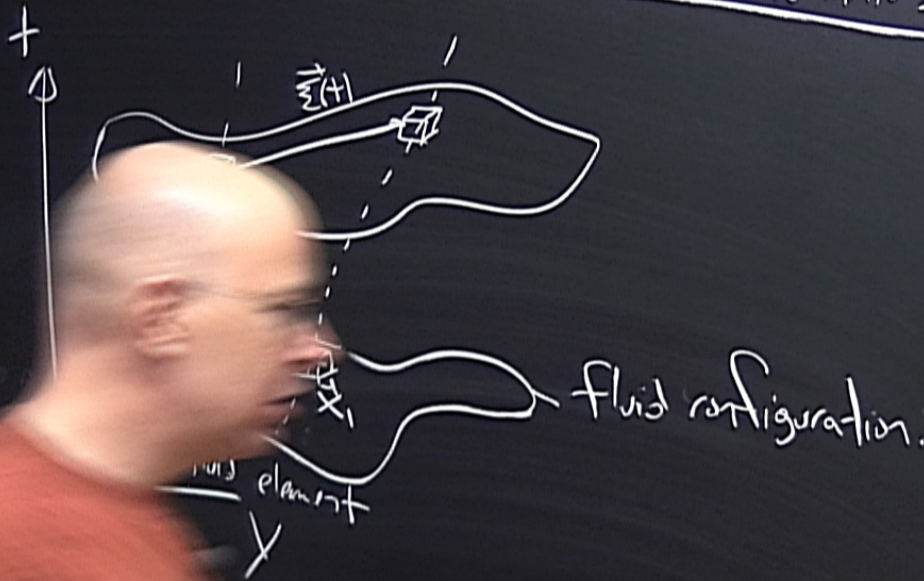
congruence: family of non-intersecting geodesics



to be continued...



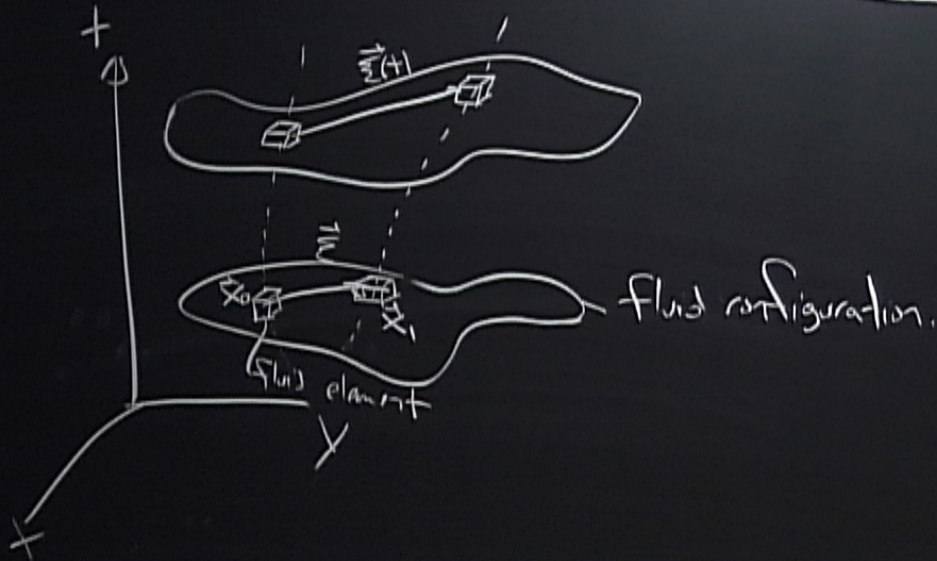
3D, Newtonian fluid mechanics



$\vec{\xi}(t)$: displacement between a given fluid element and reference fluid element

$\vec{\eta} =$

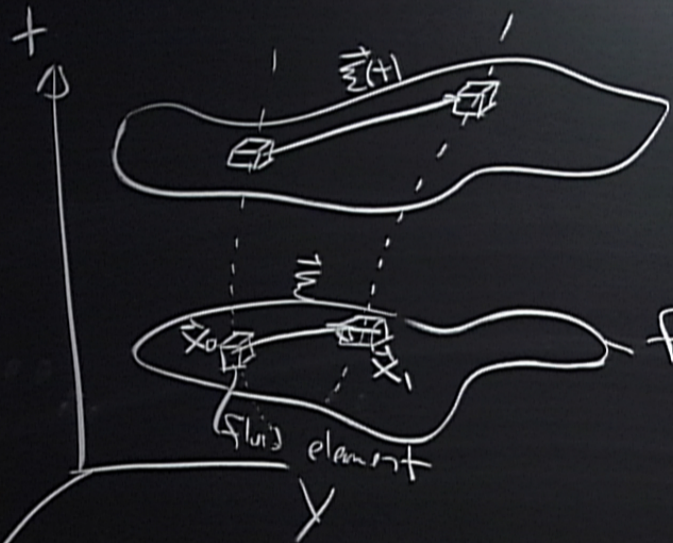
3D, Newtonian fluid mechanics



$\vec{\xi}(t)$: displacement between a given fluid element and reference fluid element

$$\vec{\eta} = \vec{X}_1 - \vec{X}_0$$

3D, Newtonian fluid mechanics

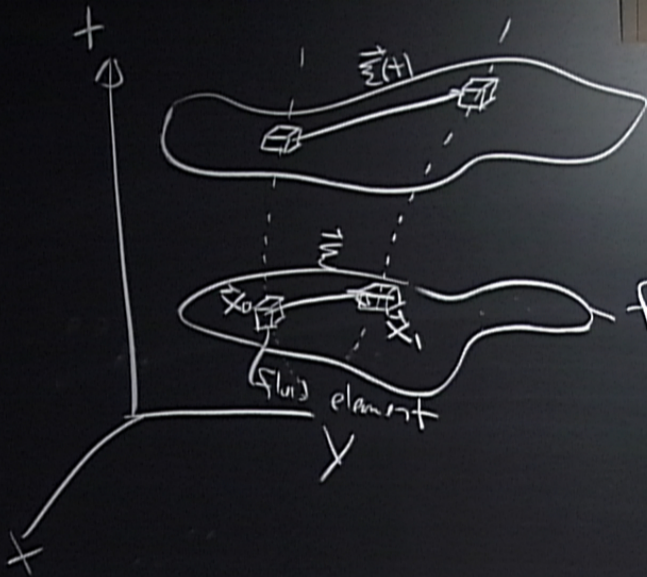


fluid configuration.

relative velocity: $\frac{d\vec{\xi}}{dt} = \vec{v}(\vec{x}_1) - \vec{v}(\vec{x}_0)$

$\vec{\xi}(t)$: displacement between a given fluid element and reference fluid element

$$\vec{\xi} = \vec{x}_1 - \vec{x}_0$$



fluid configuration.

$\vec{\xi}(t)$: displacement between a given fluid element and reference fluid element

$$\vec{\xi} = \vec{x}_1 - \vec{x}_0$$

relative velocity: $\frac{d\vec{\xi}}{dt} = \vec{V}(\vec{x}_1) - \vec{V}(\vec{x}_0)$

$$\begin{aligned} \frac{d\xi^i}{dt} &= v^i(\vec{x}_0 + \vec{\xi}) - v^i(\vec{x}_0) \\ &= v^i_{,k} \xi^k + O(\xi^2) \end{aligned}$$

$$\begin{aligned}\frac{d\xi^j}{dt} &= V^j(\vec{x}_0 + \vec{\xi}) - V^j(\vec{x}_0) \\ &= V^j_{,k} \xi^k + O(\xi^2)\end{aligned}$$

$$\begin{aligned}\frac{d\xi^j}{dt} &= B^j_k \xi^k \\ B_{jk} &= V^j_{,k}(\vec{x}_0)\end{aligned}$$

$$\begin{aligned} \frac{d\xi^j}{dt} &= V^j(\vec{x}_0 + \vec{\xi}) - V^j(\vec{x}_0) \\ &= V^j_{,k} \xi^k + O(\xi^2) \end{aligned}$$

$$\frac{d\xi^j}{dt} = B^j_k \xi^k$$

$$B^j_k(t) = V^j_{,k}(t, \vec{x}_0)$$

(evaluated at reference fluid element)

$$\begin{aligned} \frac{d\xi^j}{dt} &= V^j(\vec{x}_0 + \vec{\xi}) - V^j(\vec{x}_0) \\ &= V^j_{,k} \xi^k + O(\xi^2) \end{aligned}$$

$$\frac{d\xi^j}{dt} = B^j_k \xi^k$$

$$B^j_k(t) = V^j_{,k}(t, \vec{x}_0)$$

(evaluated at reference fluid element)

matrix without symmetries → decompose it into irreducible pieces

$$B^j_k =$$

$$\frac{d \xi^j}{dt} = B^j_k \xi^k$$

$$B_{jk}(t) = V_{jk}(t, \vec{x}_0)$$

(evaluates at reference fluid element)

matrix without symmetries → decompose it into irreducible pieces

$$B_{jk} = \underbrace{\frac{1}{3} \delta_{jk}}_{\text{trace part}} + \underbrace{\sigma_{jk}}_{\substack{\text{symmetric} \\ \text{trace-free}}} + \underbrace{\omega_{jk}}_{\text{antisymmetric}}$$

$$\frac{d\xi^j}{dt} = B^j_k \xi^k$$

$$B_{jk}(t) = V_{j,k}(t, \vec{x}_0)$$

(evaluated at reference fluid element)

matrix without symmetries \rightarrow decompose it into irreducible pieces

$$B_{jk} = \underbrace{\frac{1}{3} \delta_{jk} \Theta}_{\text{trace part}} + \underbrace{\sigma_{jk}}_{\substack{\text{symmetric} \\ \text{trace-free}}} + \underbrace{\omega_{jk}}_{\text{antisymmetric}}$$

$$\Theta \equiv \delta^{jk} B_{jk} \quad \sigma_{jk} = B_{(jk)} - \frac{1}{3} \delta_{jk} \Theta, \quad \omega_{jk} \equiv B_{[jk]}$$

$$\frac{1}{3} \delta_{jk} \Theta = \begin{pmatrix} \frac{1}{3}\Theta & 0 & 0 \\ 0 & \frac{1}{3}\Theta & 0 \\ 0 & 0 & \frac{1}{3}\Theta \end{pmatrix}$$

$$\sigma_{jk} = \begin{pmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{12} & \sigma_{22} & \sigma_{23} \\ \sigma_{13} & \sigma_{23} & -(\sigma_{11} + \sigma_{22}) \end{pmatrix}$$

$$\frac{1}{3} \delta_{jk} \Theta = \begin{pmatrix} \frac{1}{3} \Theta & 0 & 0 \\ 0 & \frac{1}{3} \Theta & 0 \\ 0 & 0 & \frac{1}{3} \Theta \end{pmatrix} \quad 1 \text{ component}$$

$$\sigma_{jk} = \begin{pmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{12} & \sigma_{22} & \sigma_{23} \\ \sigma_{13} & \sigma_{23} & -(\sigma_{11} + \sigma_{22}) \end{pmatrix} \quad 5 \text{ components}$$

$$\omega_{jk} = \begin{pmatrix} 0 & \omega_{12} & \omega_{13} \\ -\omega_{12} & 0 & \omega_{23} \\ -\omega_{13} & -\omega_{23} & 0 \end{pmatrix}$$

$$\frac{1}{3} \delta_{jk} \Theta = \begin{pmatrix} \frac{1}{3} \Theta & 0 & 0 \\ 0 & \frac{1}{3} \Theta & 0 \\ 0 & 0 & \frac{1}{3} \Theta \end{pmatrix} \quad 1 \text{ component}$$

$$\sigma_{jk} = \begin{pmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{12} & \sigma_{22} & \sigma_{23} \\ \sigma_{13} & \sigma_{23} & -(\sigma_{11} + \sigma_{22}) \end{pmatrix} \quad 5 \text{ components}$$

$$\omega_{jk} = \begin{pmatrix} 0 & \omega_{12} & \omega_{13} \\ -\omega_{12} & 0 & \omega_{23} \\ -\omega_{13} & -\omega_{23} & 0 \end{pmatrix} \quad 3 \text{ components}$$

$$\frac{d\xi^j}{dt} = B^j_k \xi^k$$

$$B_{jk}(t) = V_{j,k}(\vec{x}_0)$$

(evaluated at reference fluid element)

matrix without symmetries → decompose it into irreducible pieces

$$B_{jk} = \underbrace{\frac{1}{3} \delta_{jk} \Theta}_{\text{trace part (expansion)}} + \underbrace{\sigma_{jk}}_{\substack{\text{symmetric} \\ \text{trace-free} \\ \text{(shear)}}} + \underbrace{\omega_{jk}}_{\substack{\text{antisymmetric} \\ \text{(rotation)}}$$

$$\Theta \equiv \delta^{jk} B_{jk}$$

$$\sigma_{jk} = B_{(jk)} - \frac{1}{3} \delta_{jk} \Theta$$

$$\omega_{jk} \equiv B_{[jk]}$$

Expansion

$$\Theta = \delta_{jk} v_{j,k} = \vec{\nabla} \cdot \vec{v} = \text{fractional rate of expansion of volume of fluid elements}$$

$$\begin{pmatrix} w_{11} & 0 & 0 \\ -w_{12} & -w_{22} & 0 \\ -w_{13} & -w_{23} & 0 \end{pmatrix}$$

CAUTION

Expansion

$$\Theta = \delta_{jk} v_{j;k} = \vec{\nabla} \cdot \vec{v} = \text{fractional rate of expansion of volume of fluid elements}$$

mass conservation = $\rho \equiv \frac{\delta m}{\delta V}$ mass density

$$\rho \vec{v} \equiv \text{mass current density.}$$

$$\frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot (\rho \vec{v}) = 0$$

Expansion

$$\Theta = \delta_{jk} v_{j,k} = \vec{\nabla} \cdot \vec{v} = \text{fractional rate of expansion of volume of fluid elements}$$

mass conservation = $\rho \equiv \frac{\delta m}{\delta V}$ mass density

$\rho \vec{v} \equiv$ mass current density.

$$\frac{\partial \rho}{\partial t} + \underbrace{\vec{\nabla} \cdot (\rho \vec{v})}_{\rho \vec{\nabla} \cdot \vec{v} + \vec{\nabla} \cdot \vec{v} \rho} = 0$$

$$\frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot \vec{\nabla} \rho = -\rho \vec{\nabla} \cdot \vec{v}$$

Expansion

$$\Theta = \delta_{jk} v_{j,k} = \vec{\nabla} \cdot \vec{v} = \text{fractional rate of expansion of volume of fluid elements}$$

mass conservation = $\rho \equiv \frac{\delta m}{\delta V}$ mass density

$\rho \vec{v} \equiv$ mass current density.

$$\frac{\partial \rho}{\partial t} + \underbrace{\vec{\nabla} \cdot (\rho \vec{v})}_{\rho \vec{\nabla} \cdot \vec{v} + \vec{\nabla} \cdot \vec{v} \rho} = 0$$

$$\underbrace{\frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot \vec{\nabla} \rho}_{\frac{d\rho}{dt}} = -\rho \vec{\nabla} \cdot \vec{v}$$

As we follow a given fluid element,

$$\text{at } t = \rho(t, \vec{x})$$

$$\text{at } t+dt = \rho(t+dt, \vec{x} + d\vec{x})$$

As we follow a given fluid element,

$$\rho(t, \vec{x})$$

$$\rho(t+dt, \vec{x} + d\vec{x})$$

$$\begin{aligned} \text{total change } \delta\rho &= \rho(t+dt, \vec{x} + d\vec{x}) - \rho(t, \vec{x}) \\ &= \frac{\partial\rho}{\partial t} dt + d\vec{x} \cdot \nabla\rho + \dots \end{aligned}$$

$\frac{d\rho}{dt}$

As we follow a given fluid element,

$$\rho(t, \vec{x})$$

$$\rho(t+dt, \vec{x} + d\vec{x})$$

$$\begin{aligned} \text{total change } \delta\rho &= \rho(t+dt, \vec{x} + d\vec{x}) - \rho(t, \vec{x}) \\ &= \frac{\partial\rho}{\partial t} dt + d\vec{x} \cdot \nabla\rho + \dots \end{aligned}$$

$$\frac{d\rho}{dt} = \frac{\partial\rho}{\partial t} + \vec{v} \cdot \nabla\rho$$

As we follow a given fluid element,

$$\text{at } t : \rho(t, \vec{x})$$

$$\text{at } t+dt : \rho(t+dt, \vec{x} + d\vec{x})$$

$$\text{total change } d\rho = \rho(t+dt, \vec{x} + d\vec{x}) - \rho(t, \vec{x})$$

$$= \frac{\partial \rho}{\partial t} dt + d\vec{x} \cdot \vec{\nabla} \rho + \dots$$

$$\frac{d\rho}{dt} = \frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot \vec{v} \rho = \dots \text{ derivative}$$

$$\approx \rho_{,\alpha} v^\alpha$$

$$v^\alpha \approx (1, \vec{v})$$

As we follow a given fluid element,

$$\text{at } t : \rho(t, \vec{x})$$

$$\text{at } t+dt : \rho(t+dt, \vec{x} + d\vec{x})$$

$$\begin{aligned} \text{total change } \delta\rho &= \rho(t+dt, \vec{x} + d\vec{x}) - \rho(t, \vec{x}) \\ &= \frac{\partial\rho}{\partial t} dt + d\vec{x} \cdot \vec{\nabla} \rho + \dots \end{aligned}$$

$$\frac{d\rho}{dt} = \frac{\partial\rho}{\partial t} + \vec{\nabla} \cdot \vec{v} \rho = \text{convective derivative}$$

$$\approx \rho, \alpha U^\alpha$$

$$U^\alpha \approx (1, \vec{v})$$

shear

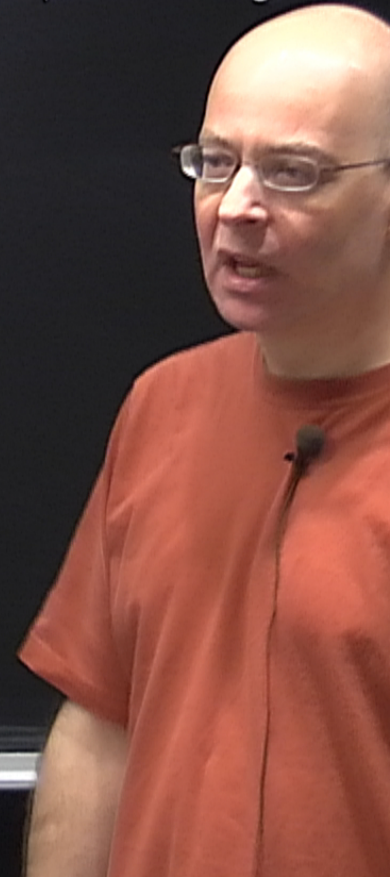
set $\Theta = 0 = \omega_{jk}$

$$\frac{d\xi^j}{dt} = \sigma^j_k \xi^k$$

take $\sigma_{12} \equiv \sigma$ to be only nonvanishing component.

$$\frac{d\xi^x}{dt} = \sigma \xi^y$$

$$\frac{d\xi^y}{dt} = +\sigma \xi^x$$



shear

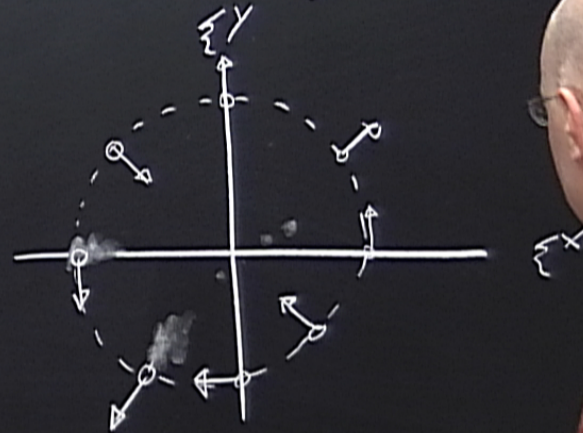
$$\text{set } \Theta = 0 = \omega_{jk}$$

$$\frac{d\xi^i}{dt} = \sigma^i_k \xi^k$$

$$\frac{d\xi^x}{dt} = \sigma \xi^y$$

$$\frac{d\xi^y}{dt} = +\sigma \xi^x$$

take $\sigma_{12} \equiv \sigma$ to be only nonvanishing component.



in shape of

shear

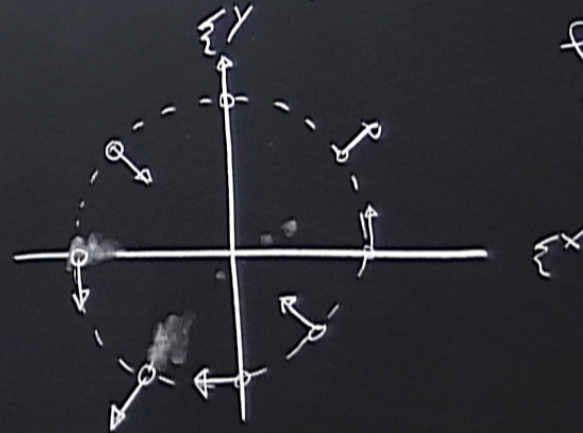
$$\text{set } \Theta = 0 = \omega_{jk}$$

$$\frac{d\xi^i}{dt} = \sigma^i_k \xi^k$$

$$\frac{d\xi^x}{dt} = \sigma \xi^y$$

$$\frac{d\xi^y}{dt} = +\sigma \xi^x$$

take $\sigma_{12} \equiv \sigma$ to be only nonvanishing component.



fluid elements in shear circle.

shear

$$\text{set } \Theta = 0 = \omega_{jk}$$

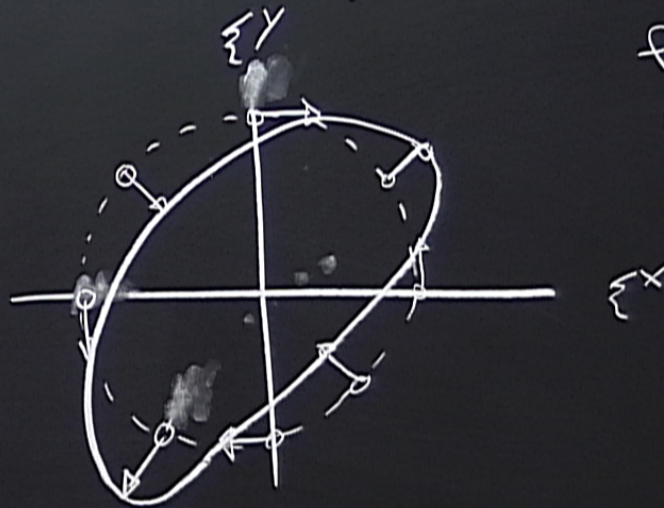
$$\frac{d\xi^i}{dt} = \sigma^i_k \xi^k$$

$$\frac{d\xi^x}{dt} = \sigma \xi^y$$

$$\frac{d\xi^y}{dt} = -\sigma \xi^x$$

take $\sigma_{12} \equiv \sigma$ to be only nonvanishing component.

fluid elements in shape of circle.



shear

set $\Theta = 0 = \omega$

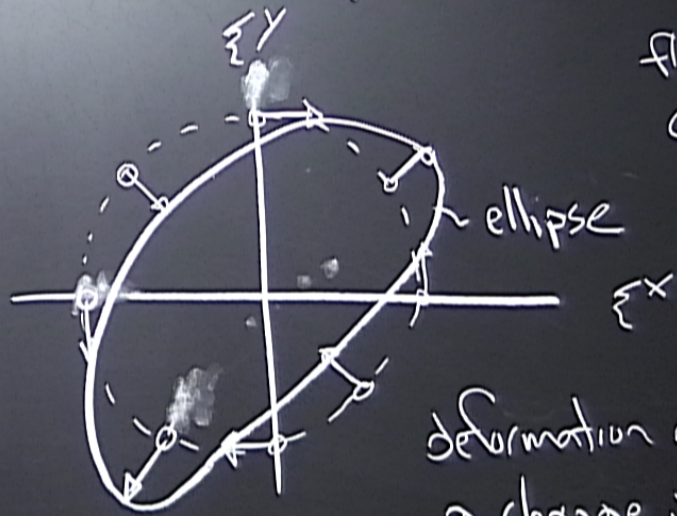
$$\frac{d\xi^j}{dt} = \sigma^j_k \xi^k$$

take $\sigma_{12} \equiv \sigma$ to be only nonvanishing component.

$$\frac{d\xi^x}{dt} = \sigma \xi^y$$

$$\frac{d\xi^y}{dt} = -\sigma \xi^x$$

fluid elements in shape of circle.



deformation of shape, without a change in volume.

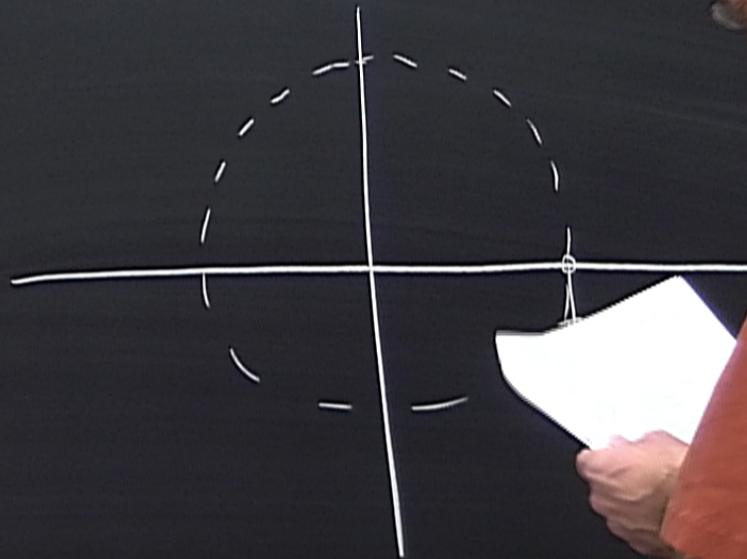
rotation

Set $\Theta = \Omega = \sigma_{jk}$

$\omega_{12} \equiv \omega$ only non vanishing on ξ^Y

$$\frac{d\xi^x}{dt} = \omega \xi^y$$

$$\frac{d\xi^y}{dt} = -\omega \xi^x$$



rotation

Set $\Theta = \mathcal{O} = \sigma_{jk}$

$\omega_{12} \equiv \omega$ only non vanishing component

$$\frac{d\xi^x}{dt} = \omega \xi^y$$

$$\frac{d\xi^y}{dt} = -\omega \xi^x$$



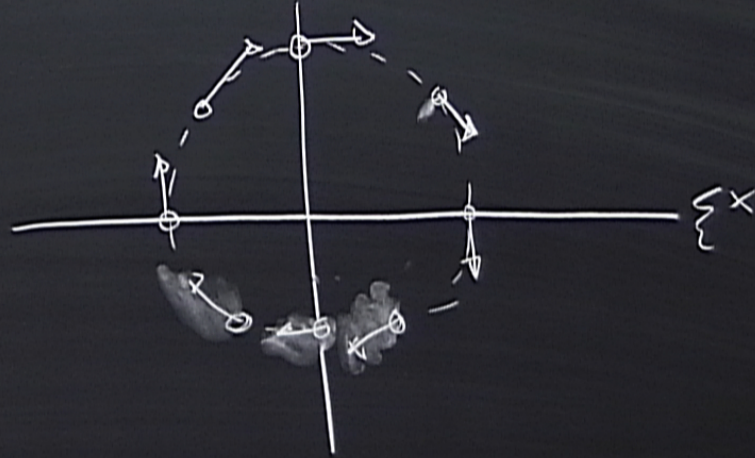
rotation

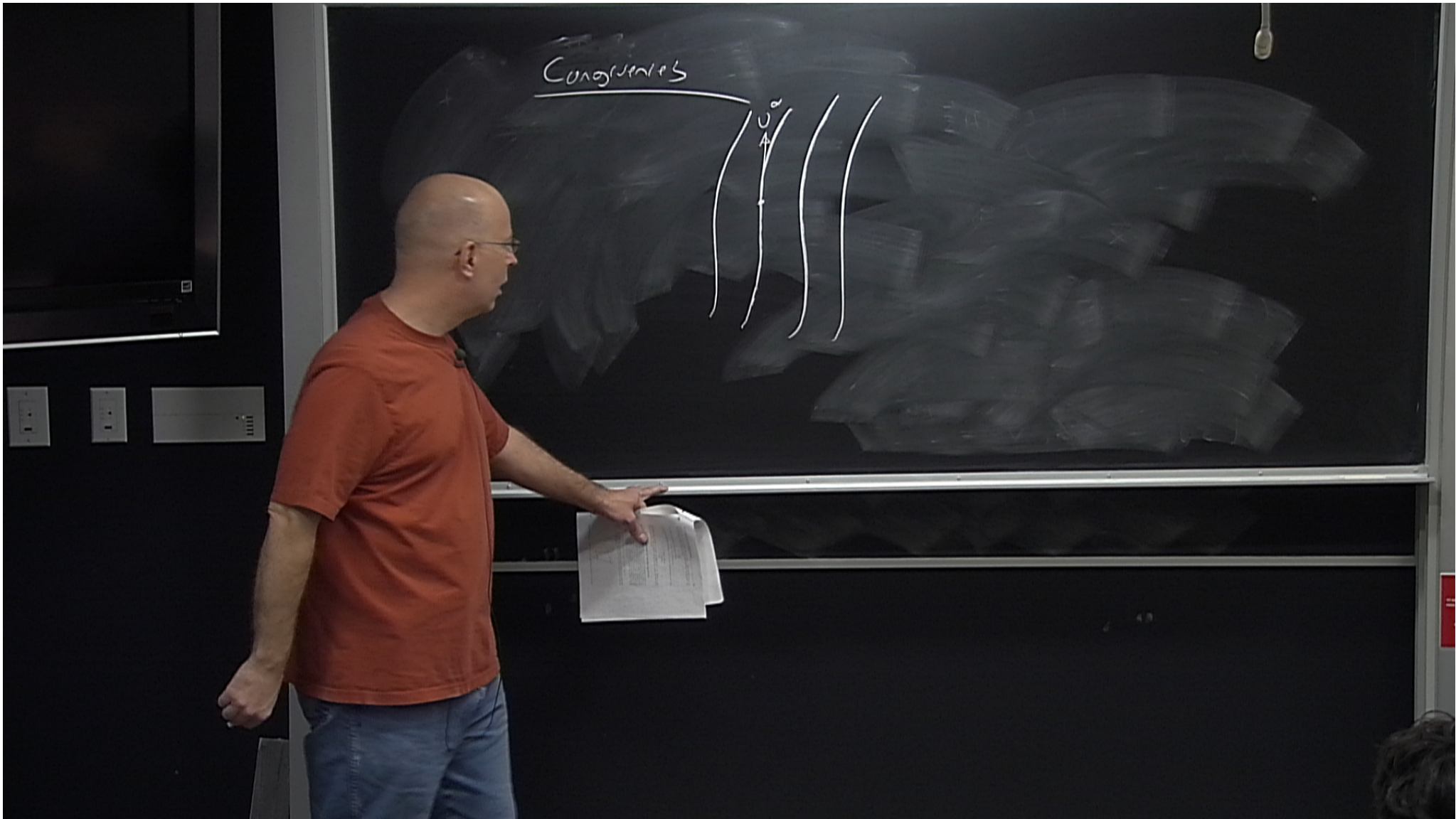
Set $\Theta = \mathcal{O} = \sigma_{jk}$

$\omega_{12} \equiv \omega$ only non vanishing component if ξ^Y

$$\frac{d\xi^x}{dt} = \omega \xi^y$$

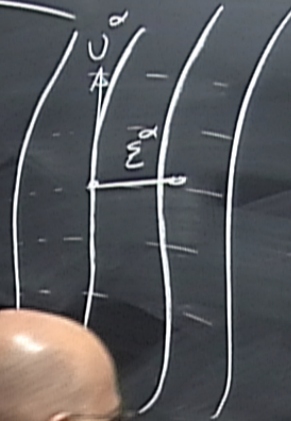
$$\frac{d\xi^y}{dt} = -\omega \xi^x$$





Congruences

timelike
geodesics



U^α : tangent vector field to congruence

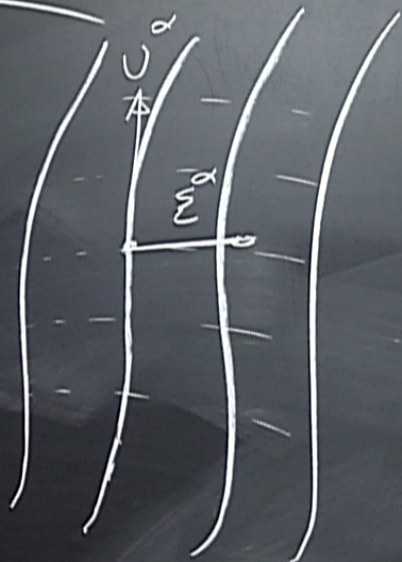
$$U^\alpha_{; \beta} U^\beta = 0$$

$$U^\alpha U_\alpha = -1$$

ξ^α : deviation vector field (tangent to cross curves)

Congruence

timelike
geodesics



U^α : tangent vector field to congruence

$$U^\alpha{}_{;\beta} U^\beta = 0$$

$$U^\alpha U_\alpha = -1$$

ξ^α : deviation vector field (tangent to cross curves)

$$\mathcal{L}_U \xi^\alpha = \mathcal{L}_\xi U^\alpha$$

$$\rightarrow \xi^\alpha{}_{;\beta} U^\beta = U^\alpha{}_{;\beta} \xi^\beta$$

$$\xi^\alpha U_\alpha = 0$$

Decomposition of $\mathcal{Z}_{\alpha\beta}$:

$$\mathcal{Z}_{\alpha\beta} = \underbrace{-U_{\alpha}U_{\beta}}_{\text{time piece}} + \underbrace{h_{\alpha\beta}}_{\text{spatial piece}}$$
$$h_{\alpha\beta}U^{\beta} = 0$$

$$h_{\alpha\beta} = \mathcal{Z}_{\alpha\beta} + U_{\alpha}U_{\beta}$$

composition of $\mathcal{Z}_{\alpha\beta}$:

$$\mathcal{Z}_{\alpha\beta} = \underbrace{-U_\alpha U_\beta}_{\text{time piece}} + \underbrace{h_{\alpha\beta}}_{\text{spatial piece}}$$
$$h_{\alpha\beta} U^\beta = 0$$

$$h_{\alpha\beta} \equiv \mathcal{Z}_{\alpha\beta} + U_\alpha U_\beta \quad \text{transverse metric}$$

$$U^\alpha h_{\alpha\beta} = U_\beta + \underbrace{(U^\alpha U_\alpha)}_{-1} U_\beta = 0$$

$$h_{\alpha\beta} U^\beta = U_\alpha + U^\alpha (U_\beta U^\beta) = 0$$

Decomposition of $\mathcal{Z}_{\alpha\beta}$:

$$h^\alpha_\rho h^\rho_\beta =$$

$$h^\rho_\beta =$$

$$\mathcal{Z}_{\alpha\beta} = \underbrace{-U_\alpha U_\beta}_{\text{time part}} + \underbrace{h_{\alpha\beta}}_{\text{spatial part}}$$

$$h_{\alpha\rho} U^\rho = 0$$

projection operator

$$h_{\alpha\beta} \equiv \mathcal{Z}_{\alpha\beta} + U_\alpha U_\beta \quad \text{transverse metric}$$

$$U^\alpha h_{\alpha\rho} = U_\rho + \underbrace{(U^\alpha U_\alpha)}_{-1} U_\rho = 0$$

$$h_{\alpha\rho} U^\rho = U_\alpha + U_\alpha (U_\rho U^\rho) = 0$$

$$\sum_{\rho} U^{\rho} = U^{\rho} \sum_{\rho} P$$

transverse metric

In a local Lorentz frame momentarily comoving with reference geodesic,

$$U^{\alpha} = (1, 0, 0, 0)$$

$$\gamma_{\alpha\beta} = \begin{pmatrix} -1 & 0 & 0 & 0 \\ 0 & +1 & 0 & 0 \\ 0 & 0 & +1 & 0 \\ 0 & 0 & 0 & +1 \end{pmatrix}$$

$$h_{\alpha\beta} = \begin{pmatrix} 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$h_{\alpha\beta} = \gamma_{\alpha\beta} + U_{\alpha} U_{\beta}$$

Behaviour of a neighbouring geodesic, relative to reference geodesic, is captured by

$$\sum_{sp}^{\alpha} \Delta P =$$

Behaviour of a neighbouring geodesic, relative to reference geodesic, is captured by

$$\sum_{\beta} U_{\beta}^{\alpha} = B_{\beta}^{\alpha} \xi^{\beta}$$
$$B_{\alpha\beta} \equiv U_{\alpha;\beta}$$

Behaviour of a neighbouring geodesic, relative to reference geodesic, is captured by

$$\sum_{\beta}^{\alpha} U^{\beta} = B_{\beta}^{\alpha} \sum^{\beta}$$

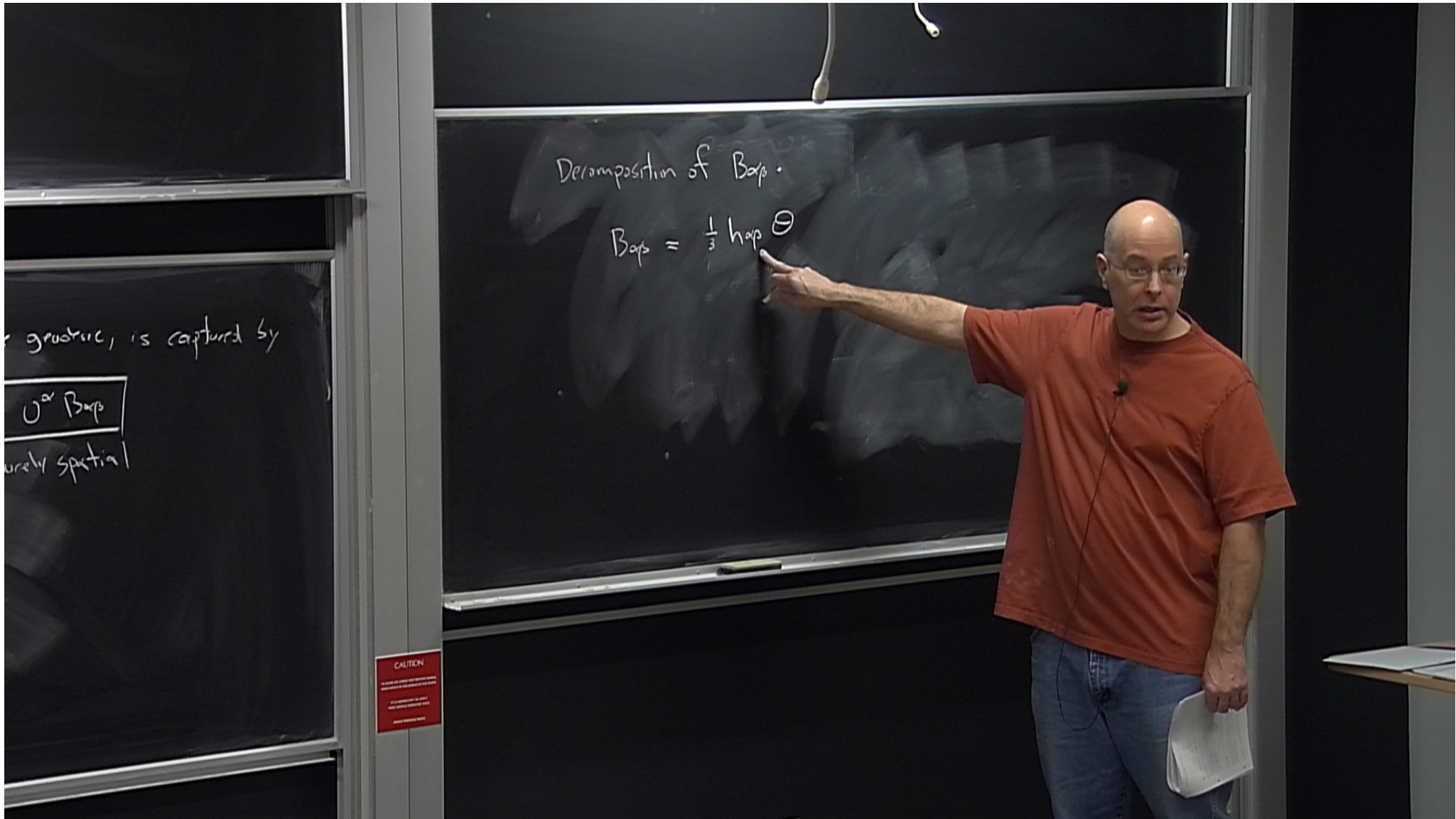
$$B_{\alpha\beta} \equiv U_{\alpha;\beta}$$

$$B_{\alpha\beta} U^{\beta} = 0 = U^{\alpha} B_{\alpha\beta}$$

$B_{\alpha\beta}$ is purely spatial

$$B_{\alpha\beta} U^{\beta} = U_{\alpha;\beta} U^{\beta} = 0$$

$$U^{\alpha} B_{\alpha\beta} = U^{\alpha} U_{\alpha;\beta} = \frac{1}{2} (U^{\alpha} U_{\alpha})_{;\beta} = 0$$



Decomposition of Baps.

$$Baps = \frac{1}{3} \text{hap } \Theta$$

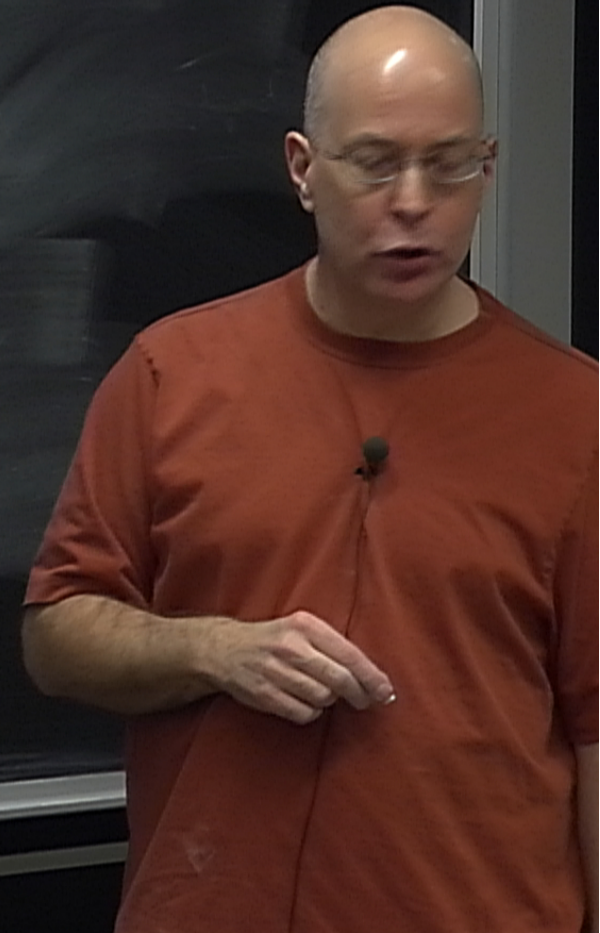
structure, is captured by

$U^{\alpha} Baps$
purely spatial

CAUTION
DO NOT TOUCH THE BOARD WHEN IT IS HOT
IT IS HOTTER THAN YOU THINK
IT IS HOTTER THAN YOU THINK
IT IS HOTTER THAN YOU THINK

Decomposition of B_{op} :

$$B_{\text{op}} = \frac{1}{3} h_{\text{op}} \Theta + \sigma_{\text{op}} + \omega_{\text{op}}$$



Decomposition of B_{op} .

$$B_{op} = \frac{1}{3} h_{op} \Theta + \sigma_{op} + \omega_{op}$$

expansion shear rotation

$$\Theta \equiv h^{op} B_{op}$$

all tensors orthogonal to u

Decomposition of $B_{\alpha\beta}$:

$$B_{\alpha\beta} = \frac{1}{3} h_{\alpha\beta} \Theta + \sigma_{\alpha\beta} + \omega_{\alpha\beta}$$

(all tensors orthogonal to U^α)

expansion shear rotation

$$\Theta \equiv h^{\alpha\beta} B_{\alpha\beta} = g^{\alpha\beta} B_{\alpha\beta} = U^\alpha_{;\alpha}$$

Decomposition of $B_{\alpha\beta}$:

$$B_{\alpha\beta} = \frac{1}{3} h_{\alpha\beta} \Theta + \sigma_{\alpha\beta} + W_{\alpha\beta}$$

expansion shear rotation

(all tensors orthogonal to U^α)

$$\Theta \equiv h^{\alpha\beta} B_{\alpha\beta} = g^{\alpha\beta} B_{\alpha\beta} = U^\alpha{}_{;\alpha}$$

$$\sigma_{\alpha\beta} \equiv B_{(\alpha\beta)} - \frac{1}{3} h_{\alpha\beta} \Theta$$

$$W_{\alpha\beta} \equiv B_{[\alpha\beta]}$$

Decomposition of $B_{\alpha\beta}$:

$$B_{\alpha\beta} = \frac{1}{3} h_{\alpha\beta} \Theta + \sigma_{\alpha\beta} + W_{\alpha\beta}$$

(all tensors orthogonal to U^α)

$$\Theta \equiv h^{\alpha\beta} B_{\alpha\beta} = g^{\alpha\beta} B_{\alpha\beta} = U^\alpha_{;\alpha}$$

$$\sigma_{\alpha\beta} \equiv B_{(\alpha\beta)} - \frac{1}{3} h_{\alpha\beta} \Theta$$

$$W_{\alpha\beta} \equiv B_{[\alpha\beta]}$$

me interpretation as fl

$$\sigma = \frac{1}{\rho V} \frac{d}{dt} \delta V$$

Decomposition of $B_{\alpha\beta}$:

$$B_{\alpha\beta} = \frac{1}{3} h_{\alpha\beta} \Theta + \sigma_{\alpha\beta} + W_{\alpha\beta}$$

(all tensors orthogonal to U^α)

$$\Theta \equiv h^{\alpha\beta} B_{\alpha\beta} = g^{\alpha\beta} B_{\alpha\beta} = U^\alpha_{;\alpha}$$

$$\sigma_{\alpha\beta} \equiv B_{(\alpha\beta)} - \frac{1}{3} h_{\alpha\beta} \Theta$$

$$W_{\alpha\beta} \equiv B_{[\alpha\beta]}$$

same interpretation as Θ

$$\Theta = \frac{1}{\delta V} \frac{d}{dt} \delta V$$

Decomposition of $B_{\alpha\beta}$:

$$B_{\alpha\beta} = \frac{1}{3} h_{\alpha\beta} \Theta + \sigma_{\alpha\beta} + W_{\alpha\beta}$$

(all tensors orthogonal to U^α)

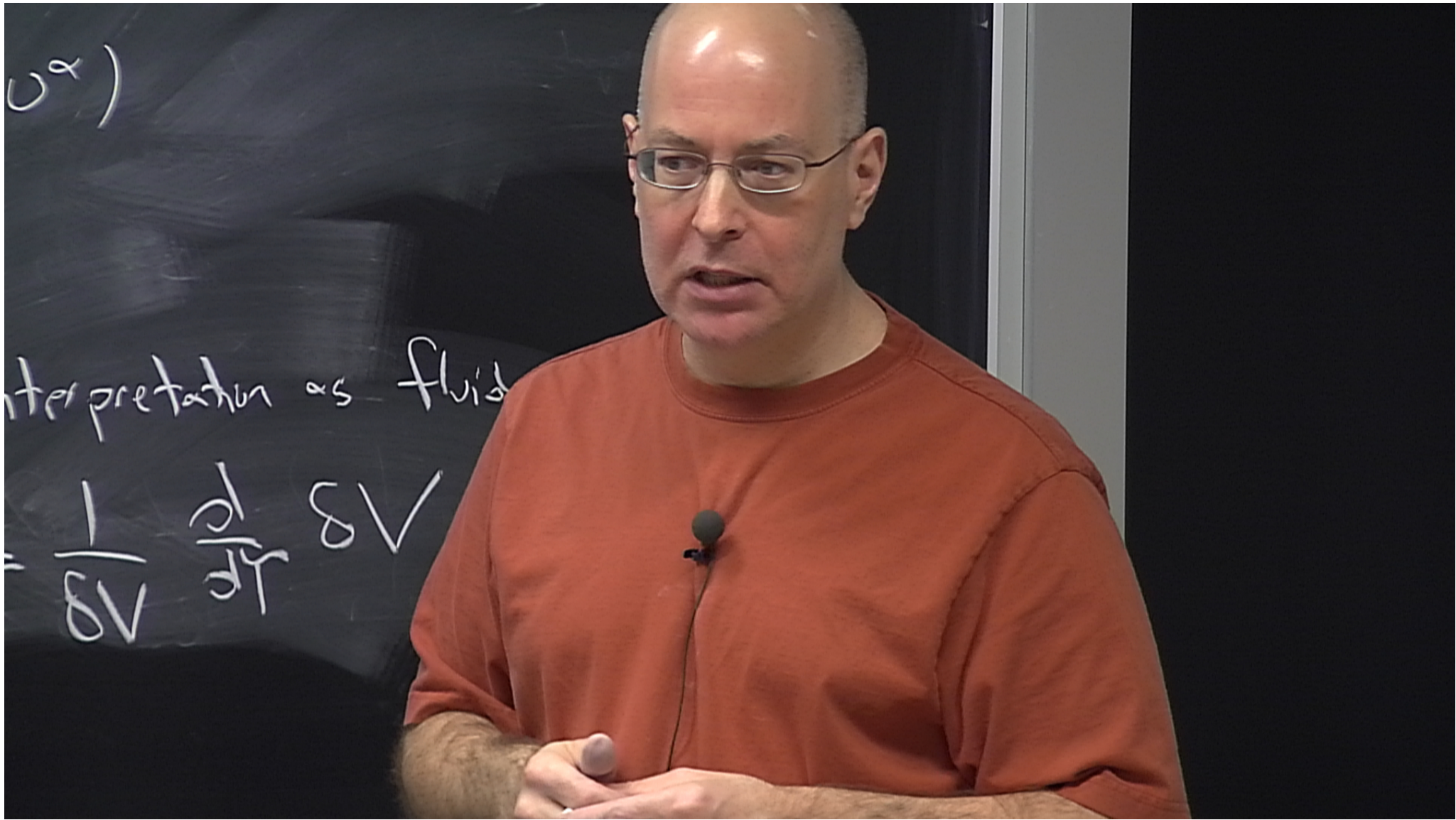
$$\Theta \equiv h^{\alpha\beta} B_{\alpha\beta} = g^{\alpha\beta} B_{\alpha\beta} = U^\alpha_{;\alpha}$$

$$\sigma_{\alpha\beta} \equiv B_{(\alpha\beta)} - \frac{1}{3} h_{\alpha\beta} \Theta$$

$$W_{\alpha\beta} \equiv B_{[\alpha\beta]}$$

same interpretation as Θ

$$\Theta = \frac{1}{\delta V} \frac{d}{dt} \delta V$$



HW 1

1-13 3 #3, #6, #9

2-5 3 #1, #3

Feb 8